CALCIUM ALUMINATE CEMENT MASS BALANCE MODEL BASED ON CaAl,O₄ HYDRATION

Neven Ukrainczyk, Juraj Šipušić, Tomislav Matusinović

FKIT, University of Zagreb, Marulicev trg 20, Zagreb, Croatia, e-mail: nukrainc@fkit.hr

1. INTRODUCTION

During the cement setting and hardening, microstructure of material and amounts of individual phases (hydraulic cement minerals, water and formed hydrates) are changing continuously^{1,2}. Knowledge of the hydration reactions and microstructure evolution is important from the viewpoint of safe usage, good durability and functionality. The hydration of CAC is highly temperature dependent³⁻⁵, yielding CAH_{10} (cement notation: C=CaO, A=Al₂O, H=H₂O) as main products at temperatures lower than 20 $^{\circ}$ C, C₂AH₈ and AH₃ at about 30 °C and C₃AH₆ and AH₃ at temperatures higher than 55 °C. CAH₁₀ and C_2AH_8 are known to be metastable at ambient temperature and convert⁶ to the more stable C₃AH₆ and AH₃ with consequent material porosity and permeability increase and loss of strength. The conversion is accelerated by temperature and moisture availability.

3. MASS BALANCE MODEL

In this work three main reactions schemes of the CA hydration at different temperatures are applied to predict the composition of cement paste. The model predictions are compared to experimental results for hydration at $T < 20^{\circ}$ C, Table 1. The model enables the quantification of volume fractions of the various hydration products, free water, unreacted cement and chemical shrinkage as a function of the degree of hydration, Figure 2. The model input variables are mass fraction of CA and $C_{12}A_7$ in cement, water to cement ratio, functions of individual reactions partition during the hydration, while stoichiometry of individual reactions, densities, and molar masses of reactants and products are known. The developed model, written for the setting of MATLAB[®] is capable to deal with simultaneous hydration reactions, both in saturated and in sealed conditions. Constant or variable individual reaction partition during the hydration can be also handled by the model.

2. EXPERIMENTAL

The CAC (iron-rich) used was taken from a regular production of Istra Cement International, Pula, Croatia. Cement pastes with w/c = 0.3, 0.4, 0.5 and 1 were prepared by mixing the distillated water and cement stabilized at required temperature. Wafers of about 10 g of cement paste were placed in small capped plastic vials and cured in thermostated bath at 5, 10, 14 and 20 °C. The composition of cement and hydrates formed had been investigated by quantitative powder X-ray diffraction (QXRD) after Chung⁷. Chemically bond water in the cement samples was determined by loss on ignition.





Figure 1. XRD analysis of cement and hardened pastes hydrated at different temperatures.

metastable hydrates are fairly broadened, indicating poor crystallinity, while that of the stable hydrated material showed good crystallinity.

Table 1. Comparison of the hydration degree obtained from measured bond water, α_{hw} with the CA QXRD analysis, α_{cA} . Sample notation in Table 1 indicates experimental variables, i.e. temperature and w/c ratio (5C04 indicates hydration at 5 °C and the w/c ration of 0.4)

Sample	<i>t</i> _h , h	<i>bw</i> , g/g	$\alpha_{\rm CA} = \alpha_{\rm active}$	$\alpha_{_{bw}}$	error, %
5C04	30	0.3278	0.62	0.640	3.20
5C04	24	0.3159	0.61	0.617	1.08
5C05	30	0.3683	0.71	0.719	1.25
5C03	30	0.2591	0.50	0.506	1.15
10C04	30	0.3380	0.65	0.660	1.50
10C05	30	0.3880	0.74	0.757	2.34
10C10	30	0.4272	0.84	0.834	-0.73
14C04	30	0.3438	0.67	0.671	0.16
14C05	30	0.3995	0.78	0.780	-0.03
20C04	30	0.3512	0.70	0.686	-2.07
20C05	30	0.4119	0.82	0.804	-1.95
20C10	30	0.4439	0.88	0.866	-1.54

where: w_{CA} - initial CA phase mass fraction in CAC,

- V_i initial volume of *i*-th phase: (H water, T total paste volume)
- w/c water to cement mass ratio,
- $(w/CA)_{tot}$ stoichiometric ratio for complete hydration,
- IP internal porosity(chemical shrinkage)

4. CONCLUSION

A relatively simple and robust cement hydration model obtained is suitable for engineering purposes. Main reaction scheme of the CA hydration at temperatures less than 20 °C can be applied to predict the composition of iron-rich calcium aluminate cement paste. Evolution of the fractional changes of chemical shrinkage, solid content and active cement should be measured to additionally validate the proposed model.

REFERENCES

- 1. Ukrainczyk, N, Matusinović, T, Šipušić, J, Microstructural Model of Calcium Aluminate Cement Hydration, *Minerals To* Materials Conference - M2M08 Bridging the Gap between Minerals and Materials: Central Metallurgical Research and Development Institute of Egypt, Cairo (2008).
- 2. Brouwers, H.J.H, The work of Powers and Brownyard revisited: Part 2, Cement Concrete Research 35 (2005) 1922 1936.
- 3. R.J. Mangabhai, Ed., Calcium Aluminate Cements, Chapman and Hall, London, 1990.
- 4. R.J. Mangabhai, F.P. Glasser, Eds, Calcium Aluminate Cements 2001, Heriot-Watt University, Edinburgh, UK, 16-19 July 2001. 5. Bensted J, Calcium aluminate cements, Structure and Performance of Cements, 2nd ed., (Eds. Bensted J, Barnes P), London, 2002.
- 6. Matusinović T, Vrbos N, Šipušić J, Rapid setting and hardening calcium aluminate cement materials, Zement-Kalk-Gips International 5 (2005) 72-79.
- 7. Chung, F.H, Quantitative interpretation of X-ray diffraction patterns of mixtures. II. Adiabatic principle of X-ray diffraction analysis of mixtures, Journal of Applied Crystallography 7 (1974) 526-531.

